Mechanical characterization of a polyester matrix composite reinforced with natural fibers from *Luffa cylindrica* Hoen

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ABSTRACT: The growing demand for renewable products has led to many studies of alternative materials. The present work describes the production of a composite based in polyester resin reinforced with fibers from the climber plant *Luffa cylindrica* and evaluates its mechanical performance. The composite was produced with two perpendicularly-crossed layers of vegetable fibers. The laminating was performed in a mold with two glass plates pressed by a hydraulic press. To characterize the properties of the produced composite, density, tensile and bending strength tests were performed. The final composite had a mean density of 1.16 g cm\(^{-3}\), making it light due to the reinforcement with vegetable fibers. Tensile and bending strengths were 13.91 and 26.70 MPa, respectively. The experimental results showed that the composite with vegetable fibers as reinforcement had lower density than the pure polyester matrix and composites produced with glass fibers. The tensile strength was higher than the polyester matrix itself, although it was still low. Also, when submitted to bending stress, the composite presented lower resistance than the matrix. Overall, the composite can be a viable alternative for non-structural applications where light materials are required such as handicrafts and office partition.

Keywords: sustainable material; vegetable fibers; mechanical properties; technical feasibility.

Caracterização mecânica de um compósito com matriz de poliéster reforçado com fibras naturais de bucha vegetal (*Luffa cylindrica* Hoen)

RESUMO: A crescente demanda por produtos renováveis tem levado a muitos estudos de materiais compósitos reforçados com fibras vegetais. A planta trepadeira *Luffa cylindrica*, conhecida popularmente como bucha vegetal, também apresenta potencial para este uso. O presente trabalho avaliou o desempenho de um compósito à base de resina de Poliéster reforçado com bucha vegetal. O compósito foi produzido com duas camadas de fibras vegetais dispostas perpendicularly entre si. A laminação foi realizada em um molde com duas placas de vidro pressionadas por uma prensa hidráulica. Como matéria-prima foi determinada a densidade e para as propriedades mecânicas, foram realizados ensaios de resistência à tração e flexão. O compósito final apresentou densidade média de 1,16 g cm\(^{-3}\), tornando-o leve devido ao reforço com fibras vegetais. As resistências à tração e flexão foram de 13,91 e 26,70 MPa, respectivamente. Os resultados experimentais mostraram que o compósito com fibras vegetais como reforço apresentou densidade menor que a matriz de poliéster pura e compósitos produzidos com fibras de vidro. A resistência à tração foi maior do que a própria matriz de poliéster. Além disso, quando submetido a tensões de flexão, o compósito apresentou menor resistência do que a matriz. No geral, o composto pode ser uma alternativa viável para aplicações não estruturais onde materiais leves são necessários, como artesanatos e paredes divisórias.

Keywords: material sustentável; fibras vegetais; propriedades mecânicas; viabilidade técnica.

1. INTRODUCTION

The replacement of unsustainable synthetic raw materials with natural ones has been a challenge in many industrial sectors, including the manufacture of composites, where the search new types of polymeric matrices and reinforcements stands out. Among the reinforcements targeted for replacement is fiberglass, which could be substituted successfully by natural fibers without affecting the strength of the composite (SANJAY et al., 2015; WAHIT et al., 2012). This could be a sustainable alternative for a wide variety of applications, ranging from packaging to the manufacture of automotive parts. The process of producing composites with natural fiber reinforcements has found wide application to make packaging materials (SARIKAYA et al., 2019).

According to Srinivas et al. (2017), polymeric composites consist of the union of a thermoplastic or thermosetting polymer reinforced with fibers. There are three types of polymeric matrix composites: particle-reinforced, fiber-
reinforced, and structural composites (SRINIVAS et al., 2017). Studies of polymeric composites reinforced with vegetable fibers have been growing rapidly. The use of natural fibers as reinforcement makes composites totally or partially recyclable or biodegradable, in addition to being inexpensive. Among the varieties of lignocellulosic fibers applied as reinforcements in composites are linen, cotton, hemp, jute, sisal, kenaf, pineapple, ramie, bamboo, and banana, among others (ELANCHENZHIAN et al., 2018).

A particularly attractive natural fiber used as reinforcement in composite materials is that of Luffa cylindrica. This plant is an herbaceous species of the Cucurbitaceae family. It is of Asian origin, and arrived in Brazil through Africans. In the Northeast region of Brazil, this plant can be found thriving spontaneously in backyards, riverbanks, and fence borders, where it grows as an annual creeper or perennial climber, reaching up to 5 meters in height (MEDEIROS, 2015; MOTA, 2016).

The fibers of Luffa cylindrica enable the production of ecological materials that do not harm the environment (MARTINEZ-PAVETTI et al., 2021). Luffa fiber-based composite materials, in addition to being environmentally safe, also provide protection from exposure to various types of toxic chemicals. The fibers are biodegradable and of high porosity, forming naturally strong entangled structure, resulting in high water absorption capacity (BABU; ARUMUGAN, 2019). The fibers are widely used in the manufacture of shoes, rugs, sponges, and mops, and also for the manufacture of value-added products, such as films and fibers for composites. Due to their lightness in weight and low cost, Luffa fibers also have uses in the manufacture of materials for the automotive industry, civil construction and medical applications, among many others (BABU; ARUMUGAN, 2019). However, in Brazil, excepting the eventual use of them as cleaning sponge, there is no large-scale or industrial utilization for this natural product.

This article reports the development of a composite with a matrix of polyester resin and reinforcement of Luffa cylindrica fibers and evaluate the physical and mechanical properties of the product.

2. MATERIAL AND METHODS

Mats of fibers from Luffa cylindrica fruits (Figure 1A) were employed for the composite assembly. The fruits were collected in the municipality of Governador Dix-Sept Rosado, Rio Grande do Norte State (5° 28′ S and 37° 31′ W), Brazil. For the production of the composite, the fruits' seeds were removed and then were washed in running water to remove the mucilage. The material was oven-dried at 80 ± 2 °C for 24 hours, cut into rectangles and pre-pressed at 0.10 MPa to obtain the flat mats depicted in Figure 1B.

The mats were placed in a mold together with crystal orthophtalic polyester resin. After assembling the matrix reinforcement, the mold was taken to a hydraulic press to start curing. Thereafter, pressed for 14 hours at 0.15 MPa. Specimens of dimensions 25 mm width x 2.7 mm thick x 25 mm length were oven-dried at 100 ± 2 °C for about 1 hour and used to determine the density of the manufactured composite using ASTM D792 (2008) standard.

The procedures described in the standard ASTM D3039 (2014) were followed for the tensile assays with 5 test specimens having dimensions of 25 mm width x 2.7 mm thickness x 240 mm length (Figure 2A).
For the bending strength determination, the specimens were submitted to the procedures described in the standard ASTM D7264 (2015). These 5 test specimens had dimensions of 13 mm width x 3.6 mm thickness x 200 mm length (Figure 2B). The mechanical assays were performed employing an EMIC DL-10000 universal testing machine (São Paulo, Brazil) equipped with a 100 KN load cell. Loading speeds of 1 and 2 mm min\(^{-1}\) were applied to the test specimens until complete fracture for the tensile and bending assays, respectively. With the values of rupture load from the machine and the dimensions of the test specimens, the maximum tensile load, deformation, and modulus of elasticity were obtained.

### 3. RESULTS

The composite produced with *Luffa cylindrica* fibers and polyester resin had mean density of 1.16 ± 0.01 g cm\(^{-3}\) (Table 1).

<table>
<thead>
<tr>
<th>Panels</th>
<th>Density (g cm(^{-3}))</th>
</tr>
</thead>
<tbody>
<tr>
<td>CP – 01</td>
<td>1.16</td>
</tr>
<tr>
<td>CP – 02</td>
<td>1.15</td>
</tr>
<tr>
<td>CP – 03</td>
<td>1.15</td>
</tr>
<tr>
<td>CP – 04</td>
<td>1.16</td>
</tr>
<tr>
<td>CP – 05</td>
<td>1.16</td>
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<tr>
<td>Mean</td>
<td>1.16</td>
</tr>
<tr>
<td>S. deviation</td>
<td>0.01</td>
</tr>
</tbody>
</table>

According to the tensile strength versus strain curves, the composite produced in this work did not reach the strength necessary for applications requiring high mechanical resistance (Figure 3).

![Figure 3](image_url)  
Figure 3. Curves obtained for the tensile strength x strain of the polyester-*Luffa* fiber composite.

As displayed in Table 2, the tensile strength of the composite reached a maximum value of 13.91 ± 0.77 MPa with strain of 0.013 ± 0.002 mm mm\(^{-1}\), and the modulus of elasticity was 1,076.57 ± 93.70 MPa.

In the bending assays, the five composite test specimens presented higher resistance compared to the tensile stress. The behavior of this property indicated by the tension x strain curves is presented in Figure 4 while the values are in Table 3. The results indicate that the composite evaluated in this work had better mechanical performance regarding bending rather than tensile stress.

The average values determined in the bending assays were 26.70 ± 3.34 MPa for strength, 0.035 ± 0.0005 mm mm\(^{-1}\) for strain, and 772.99 ± 106.38 MPa for the modulus of elasticity. The composite reached bending strength and modulus of elasticity lower than the respective values of 102.02 ± 20.88 MPa and 5,092 ± 58.00 MPa reported by Sapuan et al. (2020).

Therefore, composites of polyester reinforced with *Luffa cylindrica* have mechanical properties suitable only for non-structural applications, such as handicrafts and office partition.

![Figure 4](image_url)  
Figure 4. Curves obtained for the bending strength x strain of the polyester-*Luffa* fiber composite.

### Table 1. Density of the composite produced with *Luffa cylindrica* fibers and polyester resin.

<table>
<thead>
<tr>
<th>Panels</th>
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<td>1.16</td>
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<td>1.15</td>
</tr>
<tr>
<td>CP – 03</td>
<td>1.15</td>
</tr>
<tr>
<td>CP – 04</td>
<td>1.16</td>
</tr>
<tr>
<td>CP – 05</td>
<td>1.16</td>
</tr>
<tr>
<td>Mean</td>
<td>1.16</td>
</tr>
<tr>
<td>S. deviation</td>
<td>0.01</td>
</tr>
</tbody>
</table>

### Table 2. Values of tensile strength of the polyester-*Luffa* fiber composite.

<table>
<thead>
<tr>
<th>Panels</th>
<th>Maximum strain (MPa)</th>
<th>Maximum strain (mm mm(^{-1}))</th>
<th>Modulus of elasticity (MPa)</th>
</tr>
</thead>
<tbody>
<tr>
<td>CP – 01</td>
<td>898.87</td>
<td>0.016</td>
<td>14.23</td>
</tr>
<tr>
<td>CP – 02</td>
<td>1,020.02</td>
<td>0.014</td>
<td>14.34</td>
</tr>
<tr>
<td>CP – 03</td>
<td>1,186.28</td>
<td>0.010</td>
<td>12.04</td>
</tr>
<tr>
<td>CP – 04</td>
<td>1,096.99</td>
<td>0.014</td>
<td>15.10</td>
</tr>
<tr>
<td>CP – 05</td>
<td>1,180.67</td>
<td>0.012</td>
<td>13.85</td>
</tr>
<tr>
<td>Mean</td>
<td>1,030.29</td>
<td>0.013</td>
<td>13.91</td>
</tr>
<tr>
<td>S. deviation</td>
<td>0.002</td>
<td>0.002</td>
<td>0.77</td>
</tr>
</tbody>
</table>

### Table 3. Values determined in bending assays of the polyester-*Luffa* fiber composite.

<table>
<thead>
<tr>
<th>Test Specimen</th>
<th>Maximum strain (MPa)</th>
<th>Maximum strain (mm mm(^{-1}))</th>
<th>Modulus of elasticity (MPa)</th>
</tr>
</thead>
<tbody>
<tr>
<td>CP – 01</td>
<td>876.35</td>
<td>0.033</td>
<td>28.91</td>
</tr>
<tr>
<td>CP – 02</td>
<td>599.14</td>
<td>0.046</td>
<td>27.57</td>
</tr>
<tr>
<td>CP – 03</td>
<td>896.22</td>
<td>0.036</td>
<td>31.99</td>
</tr>
<tr>
<td>CP – 04</td>
<td>812.35</td>
<td>0.032</td>
<td>25.81</td>
</tr>
<tr>
<td>CP – 05</td>
<td>680.88</td>
<td>0.028</td>
<td>19.26</td>
</tr>
<tr>
<td>Mean</td>
<td>772.99</td>
<td>0.035</td>
<td>26.70</td>
</tr>
<tr>
<td>S. deviation</td>
<td>106.38</td>
<td>0.005</td>
<td>3.34</td>
</tr>
</tbody>
</table>
4. DISCUSSION

The density results can be considered low compared to the original density of the polyester resin, of 1.21 g cm\(^{-3}\), as reported by Sapuan et al. (2020). Pérez et al. (2018), for a hybrid composite produced with polyester, fiberglass and cayuba fibers (\textit{Aguaroup}), the final density was 1.46 g cm\(^{-3}\), and for one produced with polyester, fiberglass and abaca fibers (\textit{Musa textilis}), the density reached 1.48 g cm\(^{-3}\). The final density determined in the present work for the composite reinforced with \textit{Luffa} fibers was lower than the values of 1.30 and 1.21 g cm\(^{-3}\) found by Ferreira et al. (2020) for composites produced with epoxy-fiberglass and epoxy-fiberglass-jute fibers (\textit{Corchorus capsularis}).

Besides the low-density values found here, another positive characteristic of the composite is the biodegradability of the \textit{Luffa} fibers. Furthermore, according to Dixit et al. (2017), the use of natural vegetable fibers gives composites other properties that are attractive for industrial purposes, in particular the low cost of these fibers compared to synthetic glass, aramid, carbon and steel fibers make them preferable in the composite industry (AHMAD et al., 2015).

The low tensile strength and the variations of the samples may have been related to impurities in the fibers causing poor interaction with the polyester matrix. Other factors responsible for this poor interaction could have been air bubbles and voids in the interface areas. In their research, Faria et al. (2020) show that the lay-up influences the mechanical properties of the composite, as it provides the appearance of a greater number of bubbles and voids. In thermoplastic composites reinforced with natural fibers, the strength and modulus of elasticity depend on the properties of the polymeric matrix and the impregnation in the interface region between matrix and fibers. In composites made with fragile matrices, the mechanical stresses exerted in the material may cause high tensions in the fibers, causing low resistance (WOIGK et al., 2019).

The composite does not have high tensile strength. However, the result found is superior to the value of 8.14 ± 1.23 MPa found by Sapuan et al. (2020). When compared to the polyester resin matrix, it was found that the addition of \textit{Luffa} fiber reinforcement increased the material's tensile strength.

According to Patel et al. (2018), the increase in the percentage of natural fibers in a composite material caused an initial increase in the tensile resistance. However, after a critical point is reached, the bonding between the matrix and the fibers decreases, resulting in higher agglomeration and consequent loss of strength of the material.

Although the composite reached a better result in the bending assay, it presented variations in tension x strain curves and values similar to what was observed in the tensile assays. As occurred in the tensile assays, the variations might have been due to impurities in the material and the technique employed in the production of the composite. The chemical constituents of the natural fibers (cellulose, hemicellulose, lignin, waxes, pectin, etc.) could influence the mechanical properties of the composites including tensile, bending and impact resistance (LATIF et al., 2019).

As discussed by Latif et al. (2019), this influence arises from the presence of impurities and the chemical constituents those materials on the surface of the fibers, preventing good adherence between the reinforcement and the polymeric matrix. The interfacial and crystalline bonds are major factor affecting the mechanical properties of natural fibers. The mechanical properties are directly influenced by several factors, such as type of fiber, matrix, surface treatment and production method. Latif et al. (2019) further indicate that fibers without treatment tend to have non-cellulosic constituents and a smooth surface area, factors that cause lower mechanical interlock and incompatibility between the reinforcement of the fibers and the matrix material. SEM (Scanning Electron Micrographs) are highly recommended here for more detailed analysis of the results.

According to Elanchezhian et al. (2018), the employment of natural fibers in composites can give these materials low cost and mechanical properties desirable in civil construction and for the manufacture of partition panels, false ceilings, furniture, storage containers, tubes, bags, helmets and car and boat interior parts, among others.

5. CONCLUSIONS

The use of the \textit{Luffa} fibers as reinforcement in the production of the composite provided low density and reduced the amount of resin used in the manufacturing process, making it economically feasible to use the material for various applications. In the tensile strength tests, the composite was fragile, indicating weak adhesion between the vegetable fibers and the polyester matrix.

Although the \textit{Luffa} fibers did not provide the composite with a flexural strength higher than that of the polyester matrix, it still presented interesting results that allow the use of the material in the manufacture of products for non-structural applications. In general, the addition of \textit{Luffa} fibers resulted in good physical and mechanical properties for some uses.

6. REFERENCES


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